

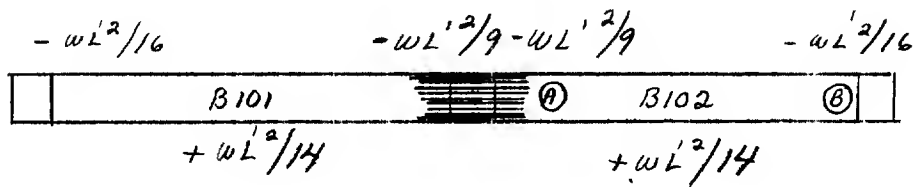
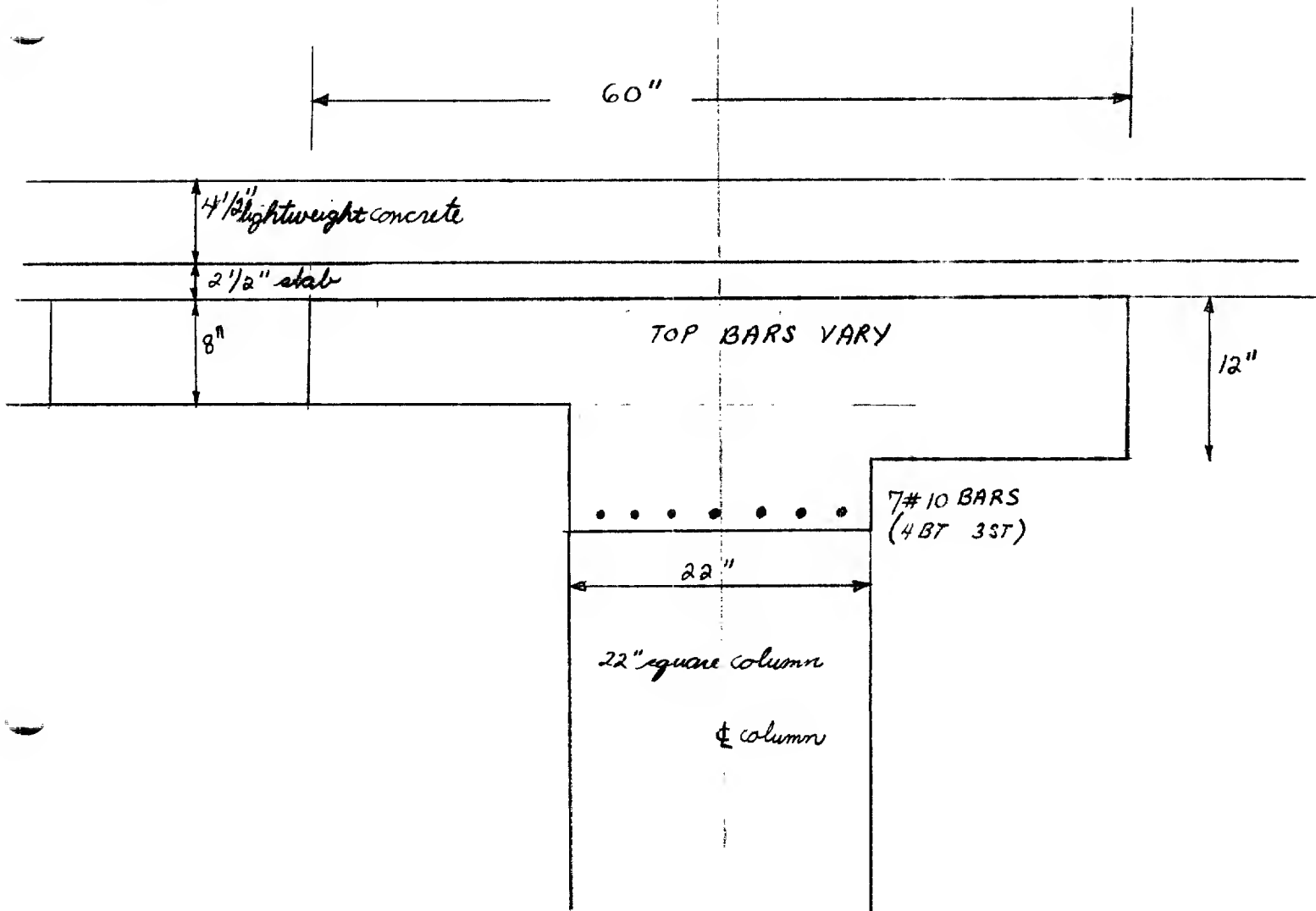
$$\begin{aligned} \text{area of corridor} &= 10 \times 20 = 200 \text{ ft}^2 \\ \text{area } \frac{41 + 26}{2} \times 60 &= 2010 \text{ ft}^2 \end{aligned}$$

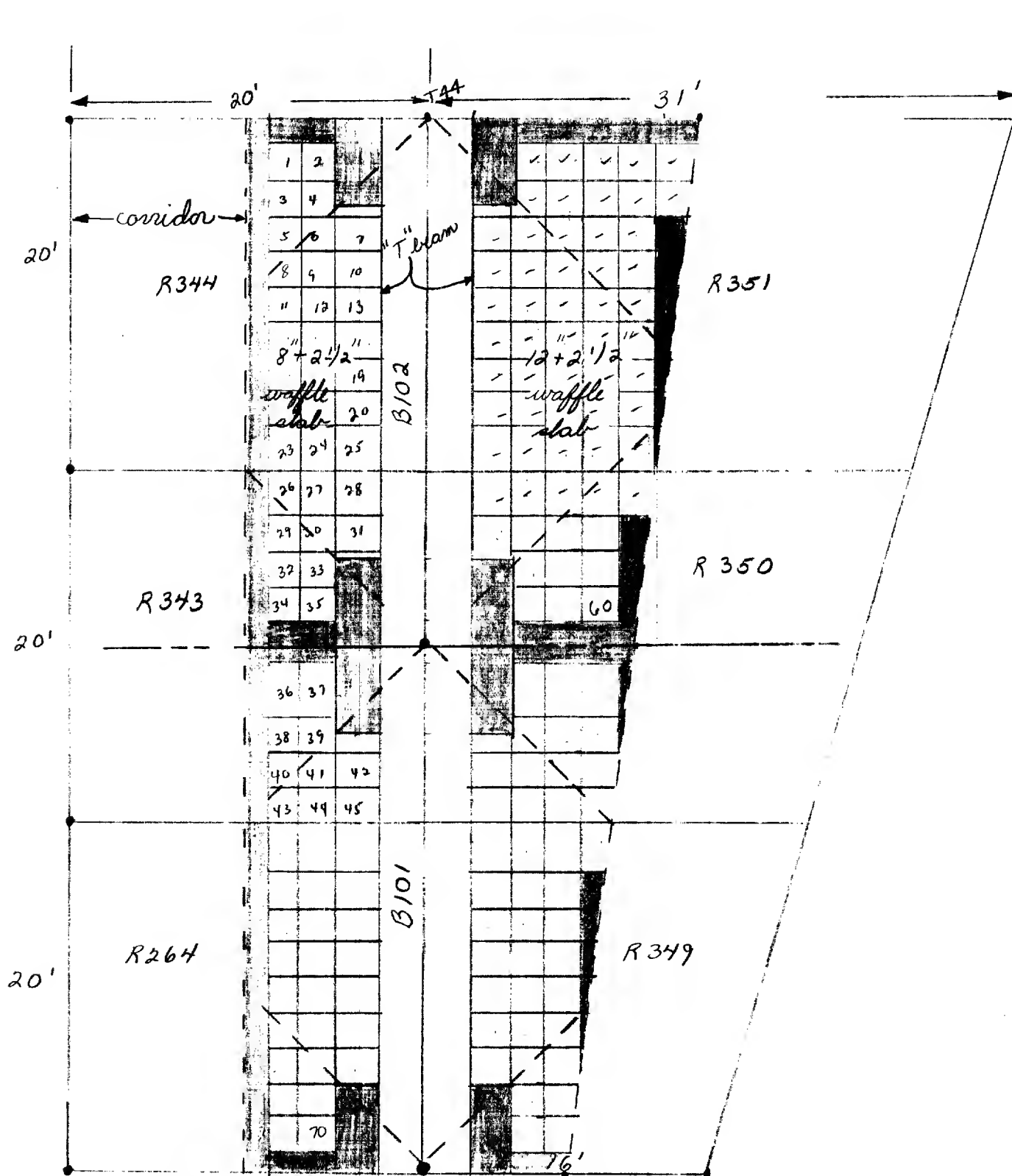
$$\begin{aligned} \text{live load allowable} &= 200 \times 100 \text{ psf} = 20,000 \\ &2010 \times 80 \text{ psf} = 160,800 \\ &\underline{180,800} \end{aligned}$$

$$\begin{aligned} 7 \text{ power files} &= 7 \times 8000 \\ &\underline{56,000} \\ &124,800 \end{aligned}$$

$$\text{net live load remaining} = \frac{124,800}{2010 + 200} = 56.5 \text{ psf}$$

Assumed "T" beam





files are $102'' \times 59\frac{3}{4}''$ $8.5' \times 4.98'$

$$8000\#/8.5 = 941.2\#/ft = .941K/ft$$

slab weights use $144\#/ft^3$ for regular concrete
use $100\#/ft^3$ for light weight concrete

$$\text{total area} = 10 \times 60 + \frac{15.5+8}{2} \times 60 = 1305\text{ft}^2$$

$$\text{weight of slab} = \frac{2.5}{12} \times 1305 \times 144 = 39150\#$$

$$\text{weight of lightweight concrete} = \frac{4.5}{12} \times 1305 \times 100 = 48938\#$$

$$\text{weight of beam} = \frac{(60 \times 8) + (9.5 \times 22) + 4(19)}{144} \times 60 \times 144 = 45900\#$$

weight of slabs $8'' + 2\frac{1}{2}''$ $12'' + 2\frac{1}{2}''$
70 panels 101 panels

$$\begin{aligned} \text{area of } 8'' + 2\frac{1}{2}'' &= 10 \times 60 = 600\text{ft}^2 \\ \text{area of } 12'' + 2\frac{1}{2}'' &= \frac{15.5+8}{2} \times 60 = 705\text{ft}^2 \end{aligned}$$

$$\text{less area of beam} = 5 \times 60 = 300$$

$$\begin{aligned} \text{area (net) of } 8'' + 2\frac{1}{2}'' &= 600 - 150 = 450\text{ft}^2 \\ \text{area (net) of } 12'' + 2\frac{1}{2}'' &= 705 - 150 = 555\text{ft}^2 \end{aligned}$$

$$\begin{aligned} [450 \times \frac{8}{12} - 70(1.41)](144) &= 28987\# \\ [555 \times 1 - 101(2.14)](144) &= 48796\# \end{aligned}$$

$$\text{area around drop panels} = (10 \times 10 \times \frac{2}{12}) 144 \times 2 \text{ panels} = 4800\#$$

$$\text{partitions + ceiling labour etc} = 20 \text{ panels} = 20 \times 1305 = 26100\#$$

partitions etc	26100
slab	39150
lightweight concrete	48938
beam	45900
remainder of slab (8")	28987
" " " (12")	48796
drop panels	<u>4800</u>
$\Sigma =$	242,671

B102 is more heavily loaded

$$\text{total area} = 1305 \text{ ft}^2$$

$$\text{area taken by B102} = 10 \times 30 + \frac{15.5 + 12}{2} \times 30 = 712.5$$

$$\text{load on B102} = \frac{712.5}{1305} \times 242,671 = 132,493 \#$$

$$\text{wght/ft} = 132.49 / 30 = 4.42 \text{ K/ft}$$

$$\text{loads due to files} = 8000 \times 3 / 30 = .8 \text{ K/ft}$$

assume $f'_c = 3000 \text{ psi}$

cover = 1.27" (dia of #10 bar) for #10 bars .875" for #7 bars

$f_c = 1350 \text{ psi}$ $f_s = 20000 \text{ psi}$

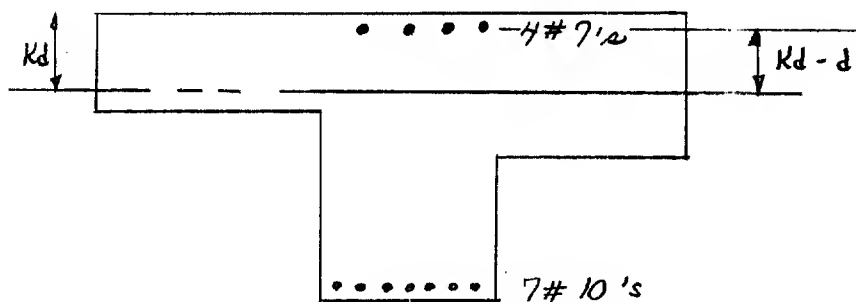
shear = 60 psi

$$\text{effective flange} \quad \frac{30 \times 12}{4} = 90"$$

$$\text{or} \\ (8 \times 2.5 \times 2) + 22 = 62" \text{ use } 60"$$

$$\text{check midspan moment} = w L'^2 / 14 = (4.42 + .8) (30 - 23/12)^2 / 14 = 296 \text{ K-ft}$$

beam at midspan



find N.A. & area about N.A.

$$b Kd \frac{Kd}{2} + 2m A's (Kd - d') = m A_s (d - Kd)$$

$$d' = .875 + .875/2 = 1.31'' \quad A's = 4(-.60) = 2.4 \text{ in}^2$$

$$d = 20 - (1.27 + \frac{1.27}{2}) = 18.1'' \quad A_s = 7(1.27) = 8.89 \text{ in}^2$$

$$60 \frac{Kd^2}{2} + 2(10)(2.4)(Kd - 1.31) = 10(8.89)(18.1 - Kd)$$

$$30Kd^2 + 48Kd - 62.88 = -88.9Kd + 1609.1$$

$$30Kd^2 + 136.9Kd - 1671.98 = 0$$

$$Kd^2 + 4.56Kd - 55.73 = 0$$

$$Kd = \frac{-4.56 \pm \sqrt{4.56^2 - 4(1)(-55.73)}}{2(1)} = 5.53''$$

$$I = \frac{b Kd^3}{3} + 2m A's (Kd - d')^2 + m A_s (d - Kd)^2$$

$$= \frac{60(5.53)^3}{3} + 2(10)(2.4)(5.53 - 1.31)^2 + 10(8.89)(18.1 - 5.53)^2 = 18283.7 \text{ in}^4$$

$$3382.2 + 854.8 + 14046.6 = 18283.7$$

$$b = \frac{M_c}{I} \quad M = \frac{6I}{C}$$

$$M_c = \frac{1350(18283.7)}{5.53} \times \frac{1}{12000} = 372 \text{ ft-Kips}$$

$$M_s = \frac{\frac{6}{m} I}{d - Kd} = \frac{\frac{20000}{10} \times 18283.7}{18.1 - 5.53} \times \frac{1}{12000} = 242.4 \text{ ft-Kips}$$

steel controls ✓

analyze B101

$$\text{load} = 242,671 - 132,493 = 110,178/30 = 3673 \#/\text{ft} = 3.67 \text{ K/ft}$$

$$M = \frac{WL'^2}{14} = \frac{(3.67 + .8)(30 - \frac{22}{12})^2}{14} = 253.3 \text{ ft-Kips}$$

if we assume B102 can carry superimposed loads
+ 80 psf

$$\text{load/ft due to 80 psf} = \frac{80 \times 712.5}{30} = 1900 \#/\text{ft} = 1.9 \text{ K-ft}$$

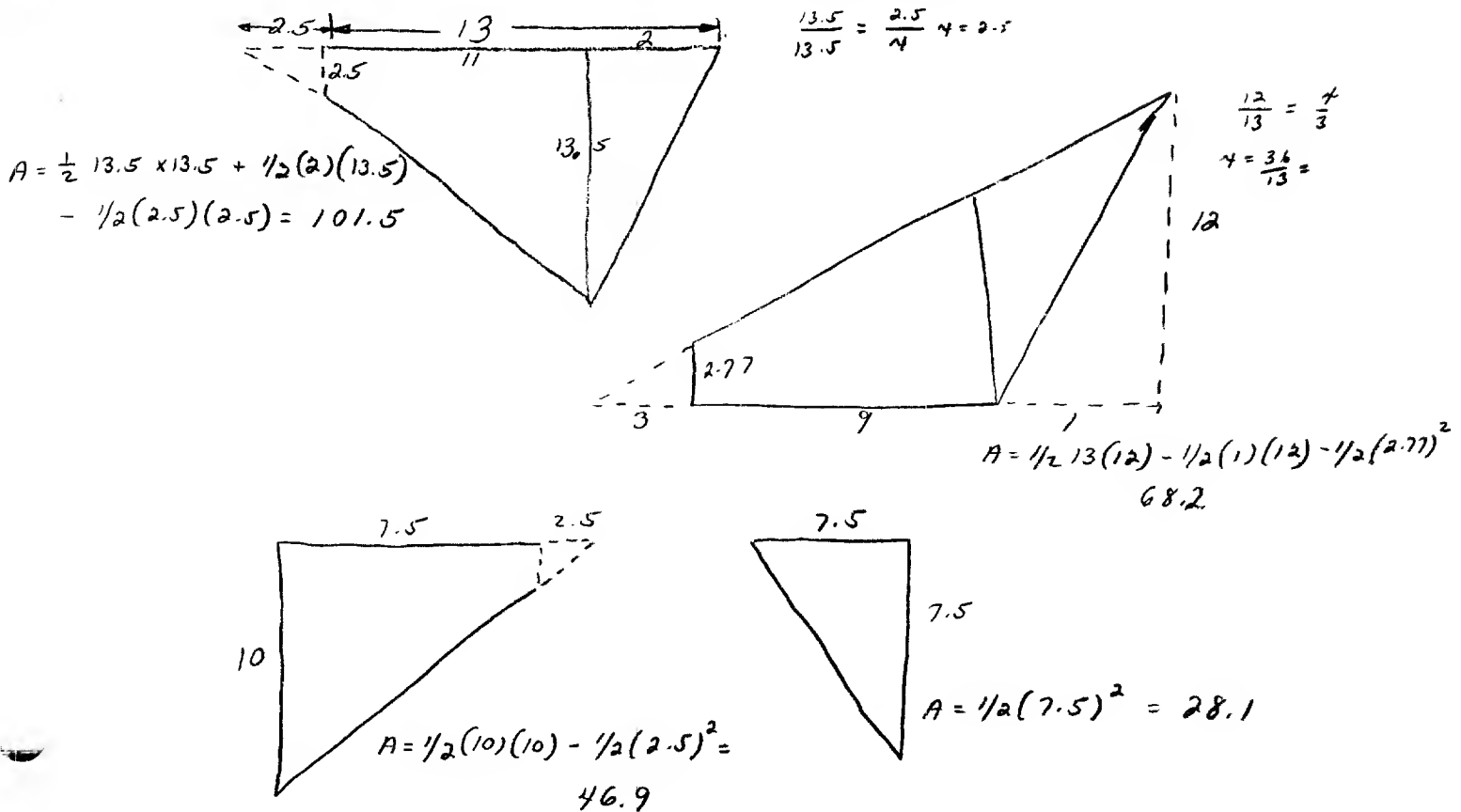
$$M = \frac{WL'^2}{4} \quad \text{max } M = 242.4$$

$$242.4 = \frac{4.42 + 1.9(30 - \frac{22}{12})^2}{4}$$

$$4 = \frac{5014}{242.4} = 20.7 ?$$

$$M = \frac{WL'^2}{21} \leftarrow \text{this cannot be}$$

try reducing loads based on 45° distribution



Area eliminated = 244.7 ft²

area of B102 = 712.5 - 244.7 = 467.8 ft²

wght = $\frac{\text{wght of beam}}{2} + \frac{467.8}{1305} \times (242671 - 45900)$

= $\frac{45900}{2} + 70536 = 93486 \#$

wght/ft = $\frac{93486}{30} \times \frac{1}{1000} = 3.12 \text{ K/ft}$

F due to 80 psf = $80(467.8)/30 \times 1/1000 = 1.25 \text{ K/ft}$

total load = $3.12 + 1.25 = 4.37 \text{ K/ft}$

$$\text{max } M = 242.4 \text{ K-ft}$$

$$242.4 = \frac{4.37 \left(30 - \frac{22}{12}\right)^2}{4} \quad 4 = 14.3 \therefore 0. K. \approx 14 \text{ which is what we should be}$$

$$M = \frac{wL^2}{14}$$

$$M = \frac{4.37 \left(30 - \frac{22}{12}\right)^2}{14} = 247.64 \text{ which checks with an allowable of } 242.4 \text{ ft-kips at midspan}$$

if files are added at midspan this would represent an increase of .8 K/ft

$$M = \frac{(4.37 + .8) \left(30 - \frac{22}{12}\right)^2}{14} = 293 \text{ ft-kips}$$

this would represent a 21 % increase over the allowable (assuming the entire 80 pef live load has been utilized)

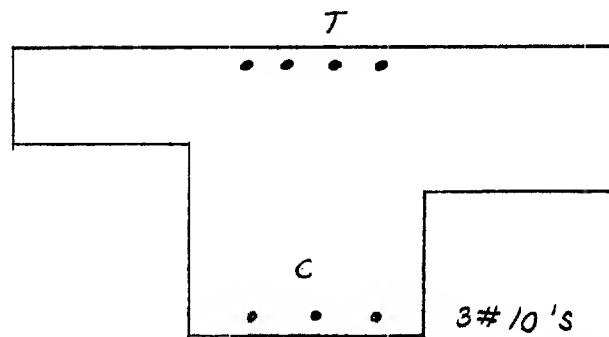
$$\text{total load assuming 0 pef live load} = 3.12 + .8 = 3.92 \text{ K/ft}$$

$$\begin{array}{r} \text{remaining} = 4.37 \\ - 3.92 \\ \hline .45 \text{ K/ft} = w \end{array}$$

$$\text{allowable live load with power files} = \frac{.45 \times 30 \times 1000}{467.8} = 29 \text{ pef}$$

say 30 pef

analyze beam over support



4 # 7's at sect A
13 # 10's at sect A
at sect B
4 # 7's
4 # 10's

$$\text{moment @ A} = -\frac{WL'^2}{9}$$

$$\text{@ B} = -\frac{WL'^2}{16}$$

$$3.12 + 1.25 + .8$$

$$455.7$$

$$3.12 + 0 + .8$$

$$345.55$$

$$3.12 + 1.25$$

$$385.2$$

$$256.4$$

$$194.37$$

$$216.7$$

$$L' = 30 - 22/2 = 28.16 \quad L'^2 = 793.361$$

capacity of beam at A

$$A_s = 4(.60) + 13(1.27) = 18.91 \text{ in}^2$$

$$A'_s = 3(1.27) = 3.81 \text{ in}^2$$

assume width = 22"

$$d' = 1.27 + 1.27/2 = 1.905$$

$$d = 20 - (1.27 + 1.27/2) = 18.1$$

$$bKd \frac{Kd}{2} + 2mA'_s(Kd - d') = mA_s(d - Kd)$$

$$22 \frac{Kd^2}{2} + 2(10)(3.81)(Kd - 1.905) = 10(18.91)(18.1 - Kd)$$

$$11Kd^2 + 76.2Kd - 145.16 = -189.1Kd + 3422.71$$

$$11Kd^2 + 265.3Kd - 3567.9 = 0$$

$$Kd^2 + 24.12Kd - 324.35 = 0$$

$$Kd = \frac{-24.12 \pm \sqrt{24.12^2 - 4(-324.35)}}{2} = 5.95 \text{ in}$$

$$I = \frac{bKd^3}{3} + 2mA'_s(Kd - d')^2 + mA_s(d - Kd)^2$$

$$= \frac{22(5.95)^3}{3} + 2(10)(3.81)(5.95 - 1.905)^2 + 10(18.91)(18.1 - 5.95)^2$$

$$= 1544.7 + 1246.8 + 27915.4 = 30707 \text{ in}^4$$

$$M_c = \frac{6I}{c} = \frac{1350(30707)}{5.95} \times \frac{1}{12000} = 581 \text{ ft-kip}$$

$$M_s = \frac{\frac{6}{n} I}{d-Kd} = \frac{\frac{20000}{10} (30707)}{18.1-5.95} \times \frac{1}{12000} = 421 \text{ ft-kip}$$

again LL must be reduced

$$\begin{array}{r} 421 \\ - 346 \\ \hline 75 \text{ K-ft for LL} \end{array}$$

$$M = \frac{wL^2}{9} \quad 75 \times 1000 = \frac{w(793.361)}{9}$$

$$w = 850.8 \#/\text{ft}$$

$$b = \frac{850.8 \times 30}{467.8} = 54.6 \text{ pcf}$$

we can therefore say + moment controls
(there is no need to check section B)

The power files can be placed in the area as proposed (with some realignment) if the LL in the surrounding area is kept to 30 pcf. This means using tables and decks but no safes, additional files and additional partitions. All existing files should be removed.

check shear

$$\text{max shear} = 1.15 W L' / 2$$

$$\text{max load} = 3.12 + .8 + .45 = 4.37 \text{ K/ft}$$

$$\text{shear} = \frac{1.15 \times 4370 (30 - \frac{22}{12})}{2} = 70,776 \#$$

$$b = F/A = 70776 / 22 \times 18.1 = 178 \text{ psi} > 60 \text{ psi}$$

stirrups required

$$\text{shear in stirrups \& bent bars} = 118 \text{ psi}$$

$$118 \times 22 \times 18.1 = 46,987.6$$

$$S = \frac{A_v f_v d}{V'} \quad 2 \#3 \text{ bars}$$

$$A_v = V' / f_v \sin \alpha \leq 1.5 b d \sqrt{f'_c} / f_v \sin \alpha$$

$$\text{diagonal bars} = 4 \#10's$$

$$S = \frac{A_v f_v d}{V'} \quad S = 2''$$

$$1.5 b d \sqrt{f'_c} / f_v \sin \alpha$$

$$2'' = \frac{2(.11)(20000)(18.1)}{V'}$$

$$1.5(22)(18.1) \sqrt{3000} / 20000 \sin 45^\circ$$

$$V' = 39,820 \#$$

$$2.31 \text{ in}^2$$

$$\text{actual} = 4 \times 1.27 = 5.08$$

$$FS = \frac{5.08}{2.31} = 2.2$$

$$2.31 = V' / f_v \sin \alpha$$

$$2.31 = V' / 20000 \sin 45^\circ$$

$$V' = 32668 \#$$

$$\leq V' = 72,488 > 46,988 \therefore \text{O.K.}$$

